

### QUAD-BAND GMSK POLAR EDGE POWER AMP MODULE

#### Package: Module, 5.00 mm x 5.00 mm x 1.00 mm



## Features

- **EDGE Large Signal Polar** Modulation Compatible
- **Power Margin for Flexible Tuning**
- GSM850 Efficiency: 54%
- **EGSM900 Efficiency: 56%**
- DCS1800 Efficiency: 49%
- PCS1900 Efficiency: 51%
- **Low Harmonic Power**
- 2.6A Current Limiter Reduces Peak Power and Current into VSWR
- **Low Switching Spectrum into** VSWR
- Industry Standard 5mmx5mm Footprint
- **Simple Application Circuitry**
- Proven PowerStar<sup>®</sup> Architecture

## Applications

- Battery Powered 2G 3G Handsets
- GMSK/EDGE Large Signal Polar Modulation Transceivers
- Multislot Class 12 Products (4 Transmit Timeslots)



Functional Block Diagram

## Product Description

The RF3225 is a high-power, high-efficiency power amplifier module with integrated power control. This device is self-contained with  $50Ω$  input and output terminals. The device is designed for use as the GMSK/EDGE power amplifier portion of the transmit chain in 2.5 and 3G transceivers supporting GMSK and/or Polar EDGE in GSM850, EGSM900, DCS, and PCS bands. The RF3225 high performance power amplifier module offers mobile handset designers a compact, easy-to-use, front end component for quick integration into multimode, multi-band systems.

#### Ordering Information



#### Optimum Technology Matching® Applied



 $\Box$  SiGe BiCMOS  $\Box$  Si BiCMOS  $\Box$  SiGe HBT

□ GaAs pHEMT  $\overline{\blacktriangle}$ Si CMOS  $\square$  Si BJT  $\Box$  GaN HEMT  $\Box$  BiFET HBT  $\square$  LDMOS

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#### Absolute Maximum Ratings





Exceeding any one or a combination of the Absolute Maximum Rating conditions may<br>cause permanent damage to the device. Extended application of Absolute Maximum<br>Rating conditions to the device may reduce device reliability.

RoHS status based on EUDirective2002/95/EC (at time of this document revision).

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Note: V<sub>RAMP\_</sub><sub>RP</sub> is defined as the V<sub>RAMP</sub> voltage required to achieve 34.5 dBm at Output load = 50Ω, V<sub>BATT</sub> = 3.6V, Temperature = 25 °C, P<sub>IN</sub> = 3 dBm











Note: V<sub>RAMP\_</sub><sub>RP</sub> is defined as the V<sub>RAMP</sub> voltage required to achieve 34.5 dBm at Output load = 50Ω, V<sub>BATT</sub> = 3.6V, Temperature = 25°C, P<sub>IN</sub> = 3 dBm











Note: V<sub>RAMP\_R</sub>p is defined as the V<sub>RAMP</sub> voltage required to achieve 32.0 dBm at Output load = 50Ω, V<sub>BATT</sub> = 3.6V, Temperature = 25°C, P<sub>IN</sub> = 3 dBm











Note: V<sub>RAMP\_R</sub>p is defined as the V<sub>RAMP</sub> voltage required to achieve 32.0 dBm at Output load = 50Ω, V<sub>BATT</sub> = 3.6V, Temperature = 25°C, P<sub>IN</sub> = 3 dBm









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## Pin Out





## Theory of Operation

#### **Overview**

The RF3225 is designed for use as the GSM power amplifier in the transmit section of mobile phones covering the GSM850, EGSM900, DCS1800, and PCS1900MHz frequency bands. The RF3225 is a high power, saturated transmit module containing RFMD's patented PowerStar® Architecture. The module includes a multi function CMOS controller, GaAs HBT power amplifier, and matching circuitry. The integrated power control loop has been optimized for use in open loop, large signal, polar 8PSK (EDGE) modulation systems. Polar EDGE operation allows designers to have the efficiency of a PowerStar® PA module as well as the enhanced data rates of EDGE modulation. A single analog voltage controls output power for GSM PCLs and ramping, as well as the amplitude component of EDGE modulation. This analog voltage can be driven from the transceiver DAC to provide very predictable power control, enabling handset manufacturers to achieve simple and efficient phone calibration in production.

### Additional Features

#### Current Limiter

During normal use, a mobile phone antenna will be subjected to a variety of conditions that can affect its designed resonant frequency. This shift in frequency appears as a varying impedance to a power amplifier connected to the antenna. As the impedance presented to the PA varies, so does the output power and current to the power amplifier. If left uncontrolled, power amplifier current can peak at high levels that starve other circuitry, connected to the same supply, of the required voltage to operate. This can result in a reset or shutdown of the mobile phone. The RF3225 contains an active circuit that monitors the current and adjusts the internal power control loop to prevent peak current from going above 2.6A. While this current limiter can limit transmitted power under situations where the antenna is operating at very low efficiency, it is typically more acceptable for users to have a dropped call than a phone reset.

#### Modes of Operation: GMSK and Polar EDGE

GMSK modulation is a constant RF envelope modulation scheme which encodes information in the phase of the signal while amplitude variation is suppressed. Since no information is included in the amplitude of the signal, GMSK transmit is not sensitive to amplitude non-linearity of the power amplifier, allowing it to operate in deep class AB or class C saturation for optimum efficiency. The GMSK power envelope may controlled by any one of a number of power control schemes.

EDGE modulation encodes information in the RF signal as a combination of both amplitude and phase. The power amplifier must be capable of re-creating both parts of the modulated signal with minimal distortion. There are several methods of creating an amplified EDGE signal. The most direct approach is to apply the EDGE modulated RF signal to a linear amplifier to boost the power. The main disadvantage to this approach is that a linear amplifier is not nearly as efficient as a saturated amplifier. Another, more complex approach is to split the EDGE signal into two components, amplitude and phase, and then recombine them in a saturated power amplifier. The benefit is that efficiency is comparable to a saturated GMSK amplifier. This method is called large signal polar modulation.

A large signal polar EDGE modulated power amplifier operates as a saturated GMSK amplifier while transmitting both GMSK or EDGE modulated signals. It is differentiated from a linear EDGE power amplifier because it always operates as a saturated amplifier. There is not a separate mode of operation that must be selected when an EDGE signal is transmitted. The RF3225 is operated in the same mode, regardless of the modulation being transmitted.





#### GMSK Operation

During GMSK transmit RF3225 operates as a traditional PowerStar® module. The basic circuit diagram is shown in Figure 1. The PowerStar® control circuit receives an analog voltage (V<sub>RAMP</sub>) which sets the amplifier output power. The PowerStar® I architecture is essentially a closed loop method of power control that is invisible to the user. The V<sub>RAMP</sub> voltage is used as a reference to a high speed linear voltage regulator which supplies the collector voltage to all stages of the amplifier. The base bias is fixed at a point that maintains deep class AB or class C transistor saturation. Because the amplifier remains in saturation at any power level, performance sensitivity to temperature, frequency, voltage and input drive level is essentially eliminated, ensuring robust performance within the ETSI power vs time mask.



#### **Figure 1. Basic PowerStar® Circuit Diagram**

The PowerStar® power control relationship is described in Equation 1 where  $V_{CC}$  is the voltage from the linear regulator and the other variables are constants for a given amplifier design and load. The equation shows that load impedance affects output power, but to a lesser degree than V<sub>CC</sub> supply variations. Since the architecture regulates V<sub>CC</sub>, the dominant cause of power variation is eliminated. Another important result is that the equation provides a very linear relationship between V<sub>RAMP</sub> and output power expressed as  $V<sub>RMS</sub>$ .

$$
P_{OUT}dBm = 10 \cdot \log \left[ \frac{\left(2 \cdot V_{CC} - V_{SAT}\right)^{2}}{8 \cdot R_{LOAD} \cdot 10^{-3}} \right]
$$

#### Equation 1: Output Power vs Voltage Relationship

The RF signal applied at RFIN of the amplifier must be a constant amplitude signal and should be high enough to saturate the amplifier. The input power range is indicated in the specifications. Power levels below this range will result in reduced maximum output power and the potential for more variation of output power over extreme conditions. Higher input power is unnecessary and will require more current in the circuitry driving the power amplifier. A higher input power may also couple to the output and will increase the minimum output power level.



#### Polar EDGE Operation

The large signal polar EDGE amplifier operates similar to a GMSK amplifier, except amplitude modulation is applied through its power control input. The polar EDGE amplifier operates in the same mode for both GMSK and EDGE transmission; but, there are several important differences between a GMSK only and a large signal polar EDGE power amplifier that require design optimization and potential performance tradeoffs.

The power control loop bandwidth of the polar EDGE amplifier must be capable of tracking the envelope of the EDGE modulation. The envelope signal may contain frequencies up to 5 times the EDGE data rate. Accurate reproduction of the power envelope is required for acceptable EVM and modulation spectrum at the output of the amplifier. The power control loop bandwidth in the RF3225 is designed to provide at least 2MHz over extreme operating conditions. Because of this, there is no internal V<sub>RAMP</sub> filter that can provide attenuation of spurious signals caused by the DAC frequency. The wide bandwidth also allows noise to enter the amplifier which can degrade the system receive band noise power performance. Filtering of the V<sub>RAMP</sub> signal external to the module may be required to meet system performance requirements.

The amplitude, AM to AM, and phase, AM to PM relationship of  $V_{RAMP}$  to the amplified RF output is a critical parameter of the large signal polar amplifier performance. Also very important are the power amplifier's amplitude and phase sensitivity to input conditions. Predictable variations can be accounted for by applying predetermined coefficients at the system level. The Power-Star® power control method is ideally suited to amplitude modulation required for the EDGE signal, because it is inherently repeatable and insensitive to many conditions. After initial calibration, the RF3225 will maintain EDGE performance over RF input drive, battery voltage, and case temperature variation.

The large signal polar power amplifier performance must be tightly coupled to the transceiver capability since the transceiver is responsible for managing and compensating for amplitude and phase non-linearity as well as the timing alignment of the amplitude and phase signals as they pass from the transceiver, through the system, to the amplifier output. Whenever the amplifier and the polar EDGE transceiver are not working together properly, modulation spectrum and EVM problems can arise.

#### Power On (Timing) Sequence

In the Power-On Sequence, there are some important set-up times associated with the control signals of the amplifier module. Refer to the logic table for control signal functions. One of the critical relationships is the settling time between TXEN going high and when V<sub>RAMP</sub> can begin to increase. This time is often referred to as the "pedestal" and is required so that the internal power control loop and bias circuitry can settle after being turned on. The PowerStar® architecture usually requires approximately  $1 - 2$  µs for proper settling of the power control loop.

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### Power Ramping

The power ramp waveform must be created such that the output power falls into the ETSI power versus time mask. The ability to ramp the RF output power to meet ETSI switching transient and time mask requirements partially depends upon the predictability of output power versus V<sub>RAMP</sub> response of the power amplifier. The PowerStar<sup>®</sup> control loop is very capable of meeting switching transient requirements with the proper raised cosine waveform applied to the V<sub>RAMP</sub> input. Ramp times between 10 and 14 µs can be optimized to provide excellent switching transients at high power levels. Shorter ramps will have a higher rate of change which will produce higher transients. Longer ramps may have difficulty meeting the time mask. Optimization needs to include all power levels as the time mask requirements change with  $P_{OUT}$  levels.

The RF3225 does not include a power control loop saturation detection/correction circuit such as the V<sub>BATT</sub> tracking circuit found in some PowerStar modules. If V<sub>RAMP</sub> is set to a voltage where the FET pass-device in the linear regulator saturates, the response time of the regulated voltage ( $V_{CC}$ ) slows significantly. Upon ramp-down, the saturated linear regulator does not react immediately, and the output power does not follow the desired ramp-down curve. The result is a discontinuity in the output power ramp and degraded switching transients. To prevent this from happening, V<sub>RAMP</sub> must be limited as the supply voltage is reduced. By maintaining V<sub>RAMP</sub> ≤0.345\*V<sub>BATT</sub>+0.26, the linear regulator will avoid deep saturation and serious switching transient degradation will be avoided.









Notes:

\* Suggested values only. Actual requirements will vary with application.

\*\*All RF paths should be designed as  $50\Omega$  microstrip or stripline.

\*\*\*NC pins on this module can be connected to ground.

\*\*\*\* T matching network is suggested because it is flexible enough for the tuning needs of most applications. Component values are not given as they are application specific.







## Evaluation Board Schematic





## Evaluation Board Layout Board Size 2.0" x 2.0" Board Thickness 0.042", Board Material RO4003 Top Layer, FR-4 Core and Bottom Layer  $P2$   $\bigcap$   $P3$  $c_1$ VBatt  $($  ) J1 J6 RF in HB RF out HB  $U1$ J4 J5  $\Box$  . RF in LB RF out LB  $\overline{\phantom{a}}$ VBand  $\Box$ TX\_EN VAPC  $\vec{\mathbf{r}}$ P1 J2 J3









## Branding Diagram



Pin 1 Indicator

Date Code:  $YY = Year$  $WW = Week$ 





## PCB Design Requirements

#### PCB Surface Finish

The PCB surface finish used for RFMD's qualification process is electroless nickel, immersion gold. Typical thickness is 2 to 5 µinch inch gold over 180 µinch nickel.

#### PCB Land Pattern Recommendation

PCB land patterns for RFMD components are based on IPC-7351 standards and RFMD empirical data. The pad pattern shown has been developed and tested for optimized assembly at RFMD. The PCB land pattern has been developed to accommodate lead and package tolerances. Since surface mount processes vary from company to company, careful process development is recommended.



## PCB Metal Land and Solder Mask Pattern



## PCB Stencil Pattern



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## Tape and Reel

Carrier tape basic dimensions are based on EIA 481. The pocket is designed to hold the part for shipping and loading onto SMT manufacturing equipment, while protecting the body and the solder terminals from damaging stresses. The individual pocket design can vary from vendor to vendor, but width and pitch will be consistent.

Carrier tape is wound or placed onto a shipping reel either 330mm (13 inches) in diameter or 178mm (7 inches) in diameter. The center hub design is large enough to ensure the radius formed by the carrier tape around it does not put unnecessary stress on the parts.

Prior to shipping, moisture sensitive parts (MSL level 2a-5a) are baked and placed into the pockets of the carrier tape. A cover tape is sealed over the top of the entire length of the carrier tape. The reel is sealed in a moisture barrier ESD bag with the appropriate units of desiccant and a humidity indicator card, which is placed in a cardboard shipping box. It is important to note that unused moisture sensitive parts need to be resealed in the moisture barrier bag. If the reels exceed the exposure limit and need to be rebaked, most carrier tape and shipping reels are not rated as bakeable at 125°C. If baking is required, devices may be baked according to section 4, table 4-1, of Joint Industry Standard IPC/JEDEC J-STD-033.

The table below provides information for carrier tape and reels used for shipping the devices described in this document.

#### Tape and Reel





**Direction of Feed**

Figure 1. 5mmx5mm (Carrier Tape Drawing with Part Orientation)